# Application of Quality by Design Principles to a Pharmaceutical Sample Using UHPLC Method Development with Modelling Technologies

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A new type of method development that uses modelling to find the "best" separation for high performance liquid chromatography (HPLC) was investigated. Principles of Quality by Design (QbD) were followed when planning the investigation. A simple Design of Experiments (DoE) with only three measured factors — gradient time, pH, and temperature — was used with different columns. The basic experiments were saved in an electronic file with the peak tracking results. After calculating a Design Space, the best prediction was compared with a confirmation run. The process delivered precise results and the method was able be transferred to a routine quality control (QC) laboratory.

For many years, a trial-and-error approach has been commonly practiced in high performance liquid chromatography (HPLC) method development — a "pick the winner" strategy. After the validation process had begun, several surprising observations were often made such as new peaks, the disappearance of other peaks, and changes in critical peak pairs. The typical response was to go back to the development process. To try to improve the separation, several test steps would be carried out, to interject quality into the method. This time-consuming process can be avoided by applying Quality by Design (QbD) principles, ensuring the quality of the method at the design stages (1). A well-established means of implementing QbD principles is to use modelling software.

To apply QbD principles to the development of HPLC methods, focus must be placed on method understanding and solid science. We took two-dimensional modelling and extended it to include a third measured factor, establishing the "Cube" (2). In a 2011 paper we demonstrated that predictions made in this way are of high quality (3). In QbD-related method development processes, trial-and-error approaches should be avoided. The best method should be developed in a planned manner, based on solid science (4). There is a great number

of different factor combinations that influence retention and resolution of the components in a mixture. The first step is column selection (5). In this study, we tested over 10 different columns and selected the Acquity BEH C18 column (Waters). To establish the number of peaks, the sample was first tested with a "scouting gradient."

Which Design of Experiments (DoE) is the simplest? The most successful design is the t<sub>G</sub>-T model (where  $t_G$  = gradient time and T = temperature). The most successful design is simple because it requires only four runs: Two gradients, t<sub>G1</sub> and t<sub>G2</sub>, with a difference of three in t<sub>G</sub> (or the slope), as was shown by Snyder and Dolan (6). We extended this design with the addition of a third factor, either pH or ternary composition,  $t_{\rm C}$  (2). The columns used had dimensions of  $50 \text{ mm} \times 2.1 \text{ mm}$  packed with 1.7-µm particles. We also used 4 and 12 min run times, with two different temperatures,  $T_1$  and  $T_2$ , here 20 °C and 50 °C. The four runs were performed following a simple batch protocol. The main points are: Not to change the injection volume during the investigation; not to interrupt the process if new peaks appear; and to use a representative sample containing all possible, even unknown, components.

The next step was to organize the received chromatograms and make

sure peak movements were realized and understood — a process called peak tracking. Every component is aligned in a horizontal line. This can be supported by the peak area of the sample, which is fairly constant in a  $t_G$ -T model. In the case of overlapping peaks, the areas are additive.

When the peak table was finished, the software calculated mathematical functions for each component. It allowed the visual examination of the resulting chromatograms, including peak movements, peak overlaps, and changes in elution order.

Compound retention behaviour is modelled so that the influence of all significant parameters (alone and in combination) is known, quantified, and visualized (2). In the HPLC method development process, relationships between parameters and their effect on the results are in this way well understood. This translates into a richer chromatographic understanding and facilitates a better scientific work.

Rather than running random test arrangements — necessary when applying statistical analysis — to fulfill QbD conditions, HPLC method development with three-dimensional models is achieved by running three t<sub>G</sub>-T models with only 12 simple experiments. From these, a large number (over 10<sup>6</sup>) of virtual experiments could be derived and the

best one found quickly. The obtained retention models were used for robustness testing, continuous quality control, and method transfer, and could serve as a fundament for Knowledge

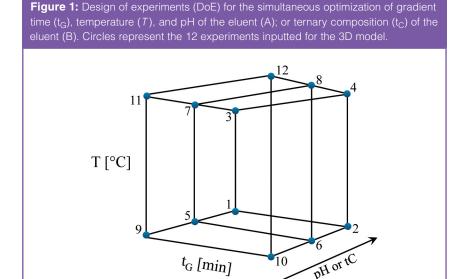
Management. In the following, we planned to compare an older method that took approximately 40 min with the new approach, based on a practical example from an industrial

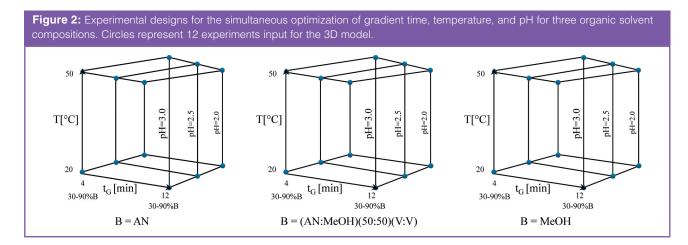
production process, using  $t_{\rm G}$ -T-pH studies to enhance column selectivity choices in ultrahigh–pressure liquid chromatography (UHPLC).

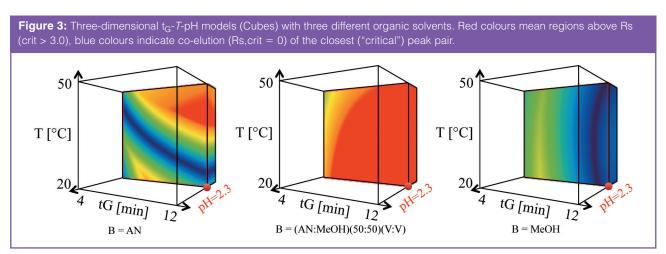
# Experimental

Eluent: The mobile phase was a mixture of acetonitrile and 5 mM ammonium dihydrogen phosphate buffer. Acetonitrile (gradient-grade), methanol, ammonium dihydrogen phosphate, phosphoric acid, and standard reference buffers (pH 2.00, 4.01, and 7.00) were obtained from Merck. For measurements, water was prepared fresh using ELGA Purelab UHQ water. The buffer was filtered before use on a regenerated cellulose filter membrane, 0.2-µm pore size (Sartorius).

Samples contained 10–30 µg/mL amlodipine and its *European Pharmacopeia* (*Ph.Eur.*) impurities (A, B, D, E, F, G, H) and 1 mg/mL amlodipine spiked at 0.1% (European Directorate for the Quality of Medicines & HealthCare).







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Figure 4: Predicted chromatograms are showing that in all three eluent compositions robust separations are possible at pH 2.3 ( $t_G = 8 \text{ min, } 30-70\% \text{ B}$ ,  $T = 40 \,^{\circ}\text{C}$ ).

Figure 5: Four-dimensional  $t_{G^-}$ 7-ternary model (fourth dimension was pH) and  $t_{G^-}$ 7-sheet with "working point".

Working Point

T [°C]  $t_{G^-}$ 1 Working Point  $t_{G^-}$ 1 To  $t_{G^-}$ 1 To  $t_{G^-}$ 2 To  $t_{G^-}$ 2 To  $t_{G^-}$ 2 To  $t_{G^-}$ 3 To  $t_{G^-}$ 4 T

Time (min)

B = (AN:MeOH)(50:50)(V:V)

**Equipment and Software:** An Acquity UHPLC system (Waters), Empower software, and Acquity BEH C18 50 mm × 2.1 mm, 1.7-μm column (Waters) were used. This system had a 5-μL injection loop and a 500-nL flow cell. The dwell volume of the system was measured to be 0.125 mL. The pH was measured with a MP 225 pH meter (Mettler Toledo).

Time (min) B = AN

Method development and method modelling were performed using DryLab 2010 HPLC/GC optimization software, consisting of the DryLab Core-module v.3.9, PeakMatch v.3.6, and the 3D-Resolution Space feature called the "Cube" (Molnár-Institute).

## **Results and Discussion**

The problem of older HPLC methods, which may be available in

pharmacopeias, is that the columns are often of an old type which are sometimes not available anymore. Furthermore, many old methods are very slow. This causes, in a modern pharmaceutical environment, great delays in the production of certain drugs. We need an easy replacement for older methods to be able to use more modern instrumentation and columns. We tried, in our case, to reduce the analysis time of the old method from 40 min to hopefully less than 10 min.

Time (min)

B = MeOH

There were several approaches to the selection of the proper design in the literature (7,8). As DoE we use the one shown in Figure 1 with 12 experiments (2). The advantage here is the fast evaluation of the sample using gradients. The creation of a cube was based on

reversed-phase gradient elution (9) with the columns mentioned above, and was done in 3–4 h, representing more than 10<sup>6</sup> virtual experiments. Column selectivity was evaluated quickly under consideration of both stationary and mobile phase influences.

Experimental design for simultaneous optimization of gradient time, temperature, and pH and ternary eluent composition t<sub>C</sub>, required 12 experiments, as illustrated in Figure 2 (2). Two basic gradients with different rates (4 and 12 min gradient time, in a range of 30-90% B) were carried out at two different column temperatures (20 and 50 °C). The mobile phase "A" consisted of 5 mM ammonium dihydrogen phosphate buffer (pH = 2.0, 2.5, and 3.0), "B1" wasacetonitrile, and "B2" was methanol. The flow-rate was at 0.5 mL/min. The injection volume was 1 µL.

We were able to create a four-dimensional model, as we prepared three cubes in identical pH ranges, but with three different ternary eluents, methanol, acetonitrile, and 50:50 (v/v) (methanol:acetonitrile). Then we selected a pH value, where our separation was robust in terms of pH with little risk of losing efficiency. From the three cubes we exported 3 × 4 chromatograms as the reference points of a new cube.

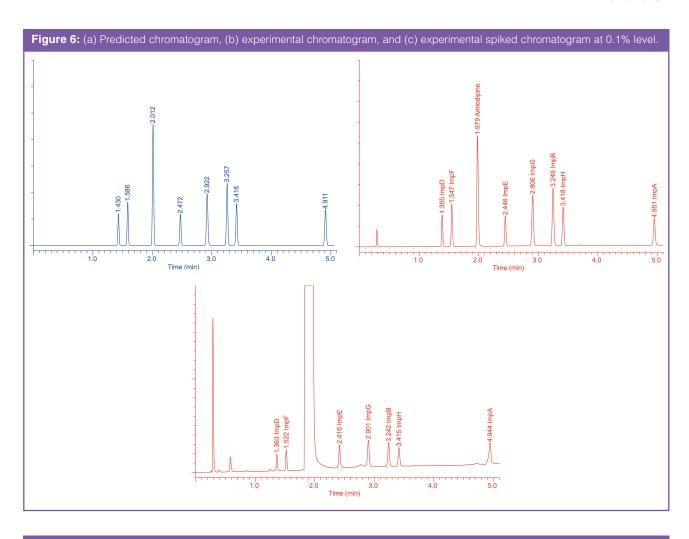
Predicted optimum parameters were:  $t_G = 5$  min; gradient range: 30–70% B; T = 40 °C; pH = 2.3; and ternary composition ( $t_C$ ) = 75:25 (v/v) acetonitrile:methanol.

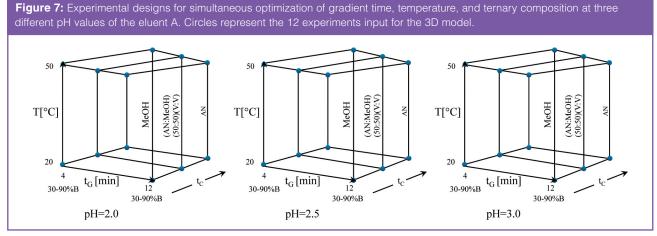
From three cubes we selected those  $t_G$ -T sheets that belong to pH 2.3, as shown in Figure 3.

In Figure 4 we can see that the system is robust for pH changes, but not robust at two ternary eluents: With 100% acetonitrile (AN) the resolution between ImpG and ImpB is small. In the case of methanol (MeOH) the components ImpE and ImpG exhibit partial overlaps. Using 50:50 (v/v) methanol:acetonitrile as eluent B, we achieve a much better separation of the critical impurity components.

The next step was the selection of the "working point" at 40 °C and  $t_{\rm G}$ : 5 min (30–90% B) where B was 75:25 (v/v) acetonitrile:methanol.

Finally, the conformation of the prediction in Figure 6(a) revealed an excellent separation of all components, which could be well confirmed, as shown in practice with a mix of the





standards in Figure 6(b) and with the drug product in Figure 6(c).

The precision of the predicted vs. modelled experiments are showing only small deviation of a few hundredths of a min (11–13). Looking at the last two peaks, the retention times are 3.145 vs. 3.148 min, a difference of 0.003 min and 4.944 vs. 4.911, a difference of 0.033 min.

After these steps we turned the process in the experimental design around and produced first three Cubes with a constant ternary composition region, but with three different pH values. For the creation of a new Cube we selected one ternary composition, and from the three Cubes we exported 12 runs. We received at the same working point the same separation

as in the first part of the study (see Figures 7–10).

In Figure 9, the "working point" was selected at  $t_{\rm G}=5$  min and T=40 °C and pH 2.3. The predicted chromatogram has a run time of less than 5 min.

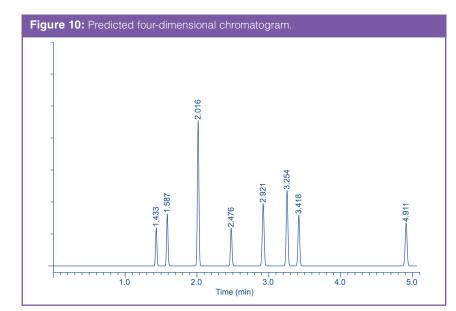
Using the software we were also able to increase the speed of the separation by modelling the flow rate.

Figure 8: Three-dimensional t<sub>G</sub>-7-ternary models (Cubes) with three different pH values (2.0, 2.5, and 3.0). Red colours mean regions above Rs (crit > 3.0); blue colours indicate coelution (Rs, crit = 0) of the closest ("critical") peak pair. 50 50 50 T[°C] T [°C] T [°C] 20 20 20 (15:25) W.W tG [min] tG [min] tG [min] 12 12 12 pH=2.0 pH = 3.0pH = 2.5

Figure 9: Four-dimensional  $t_G$ -T-pH model (fourth dimension was ternary composition) and  $t_G$ -T-sheet with "working point".

Working Point

T [°C]  $t_G[min]$   $t_G[min]$ 



With a faster gradient time ( $t_{\rm G}=2$  min) and an increased flow rate of 0.8 mL/min, we were able to further reduce the analysis time to less than 1.8 min.

The new predicted parameters are:  $t_G=2$  min; gradient range 30–90% B; flow rate: 0.8 mL/min;  $T=40\,^{\circ}\text{C}$ ; and pH = 2.3; and with  $t_C=75:25\,\text{(v/v)}$ 

acetonitrile:methanol we receive the prediction shown in Figure 11(a) with the correspon ading confirmation run in Figure 11(b). In this way, the analysis time could be reduced to less than 1.8 min.

The *Ph.Eur.* method is very long and this specifies only three impurities

(14) while our method takes less than two minutes and seven impurities are specified (see Figure 12).

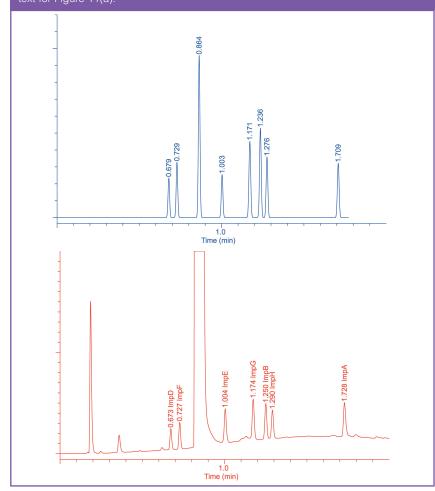
# **Summary**

In this study, we were able to reduce the analysis time of a pharmaceutical preparation from 40 min to below 1.8 min using UHPLC instrumentation, modern short UHPLC columns, and modelling software. With the short analysis time the production of the drug is faster and more economical than in the past. The use of the modelling software allowed us to fulfill QbD criteria for the method, increasing flexibility in a routine operation. Retention and critical resolution phenomena became more transparent than they were before. Method transfer is also easier using the Knowledge Management protocol described in the paper. In case of renewing older methods we recommend the above technology because of its reliability and speed.

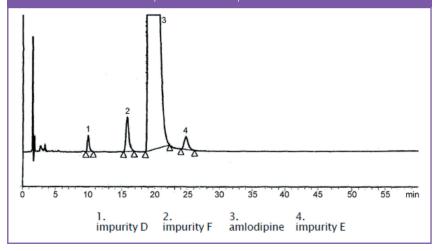
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**Figure 11:** (a) Predicted chromatogram with increased flow rate to 0.8 mL/min; (b) Experimental spiked chromatogram at 0.1% level. Conditions are as described in the text for Figure 11(a).



**Figure 12:** Chromatogram of amlodipine and its impurities from the *European Pharmacopeia* 7.4, Amlodipine besilate 04/2012:1491 p.4275-4276. The *Ph.Eur.* method is very long and specifies only three impurities, while our method has a run time of less than 2 min and specifies seven impurities.



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